

HALEY & ALDRICH, INC. 6500 Rockside Road Suite 200 Cleveland, OH 44131 216.739.0555

MEMORANDUM

16 October 2016 File No. 40616-108

SUBJECT: Initial Run-on and Run-off Control Plan Associated Electric Cooperative, Inc. New Madrid Power Plant – Utility Waste Landfill New Madrid, MO

Haley & Aldrich, Inc. (Haley & Aldrich) was retained by Associated Electric Cooperative, Inc. (AECI) to develop this Initial Run-on and Run-off Control Plan for the coal combustion residuals (CCR) Utility Waste Landfill (UWL) at the New Madrid Power Plant (NMPP) to comply with the requirements of the U.S. Environmental Protection Agency (USEPA) 40 CFR Parts 257 and 261 "Hazardous and Solid Waste Management System; Disposal of Coal Combustion Residuals From Electric Utilities" (CCR Rule) section §257.81. The existing conditions of the UWL active portion (Phase I) run-on and run-off control system has been reviewed and associated stormwater modeling and analysis performed to meet the requirements of the Run-on and Run-off Control System Plan (Plan) requirement of CCR Rule Section §257.81 as described in the sections below. Once additional phases become active, this Plan will be updated accordingly.

<u>§257.81(a)</u>: The owner or operator of an existing or new CCR landfill or any lateral expansion of a CCR landfill must design, construct, operate, and maintain:

<u>§257.81(a)(1)</u>: A run-on control system to prevent flow onto the active portion of the CCR unit during the peak discharge from a 24-hour, 25-year storm;

The UWL is located approximately 1.7 miles southwest of the New Madrid Power Plant, in New Madrid County, Missouri. Phase I of the Landfill is currently active, with Phase III being an existing phase of the landfill not currently receiving CCR as of the date of this Plan. The UWL was constructed with a perimeter berm around each side above existing grades. The perimeter berm, which also serves as an access road, is roughly 6 feet in height when measured to the existing topography outside of the UWL and prevents run-on to the active portion of the UWL. It is not feasible for the 24-hour, 25-year storm (6.62 inches) to flow over the berm and into the active portion of the UWL.

<u>\$257.81(a)(2)</u>: A run-off control system from the active portion of the CCR unit to collect and control at least the water volume resulting from a 24-hour, 25-year storm.

Stormwater runoff from the UWL is managed by the perimeter berms. Stormwater is conveyed in ditches that drain from a high point in the northeast corner of the UWL towards the low point

in the southwest corner. Stormwater is collected in the southwest corner of the landfill footprint, in accordance with the intended design, and passes through the landfill berm and into a clay-lined ditch via a 24-inch HDPE pipe. The ditch drains to the east and empties into a clay-lined sedimentation pond via a 24-inch HDPE pipe. AECI maintains a water level in the pond at approximately El. 281 by periodically pumping water to the existing CCR impoundments. AECI also pumps water to the existing CCR impoundments throughout large storm events to limit peak water surface elevations.

Haley & Aldrich analyzed the existing stormwater run-on and run-off for the UWL for the 24hour, 25-year storm event in HydroCAD 10.00-15. The rainfall data for the analysis was obtained from NOAA Atlas 14 for the site. The rainfall for the 24-hour 25-year storm event was 6.62 inches. The Soil Conservation Service Type-II rainfall distribution pattern was used to distribute the total rainfall over a 24-hour period. Appendix A includes rainfall data used in the hydrologic model. The existing conditions and drainage areas for the unit are shown in Figure 1.

The results of the HydroCAD model are included in Appendix B. The results of the model indicate that the stormwater conveyance system for the UWL adequately handle the volume of the 24-hour, 25-year storm event. The pipe from the UWL footprint to the conveyance ditch and the pipe from the ditch to the sedimentation pond convey stormwater without causing a peak water surface elevation above the landfill and ditch berm elevations. Additionally, the sedimentation pond collects and controls the water volume resulting from the 24-hour, 25-year storm event below berm elevations.

<u>§257.81(b)</u>: Run-off from the active portion of the CCR unit must be handled in accordance with the surface water requirement under §257.3-3.

<u>§257.3-3(a)</u>: For purposes of section 4004(a) of the Act, a facility shall not cause a discharge of waters of the United States that is in violation of the requirements of the National Pollutant Discharge Elimination System (NPDES) under section 402 of the Clean Water Act, as amended.

<u>§257.3-3(b)</u>: For purposes of section 4004(a) of the Act, a facility shall not cause a discharge of dredged material or fill material to waters of the United States that is in violation of the requirements under section 404 of the Clean Water Act, as amended.

<u>§257.3-3(c)</u>: A facility or practice shall not cause non-point source pollution of waters of the United States that violates applicable legal requirements implementing an areawide or Statewide water quality management plan that has been approved by the Administrator under section 208 of the Clean Water Act, as amended.

Stormwater from the UWL is managed on-site for the 24-hour, 25-year storm event, and the only discharge from the sedimentation pond is pumped to existing CCR impoundments. Those impoundments either discharge via evaporation or through permitted NPDES outfalls.



<u>§257.81(c)(1)</u>: Contents of plan. The owner or operator must prepare initial and periodic run-on and run-off control system plans for the CCR unit according to the timeframes specified in paragraphs (c)(3) and (4) of this section. These plans must document how the run-on and run-off control systems have been designed and constructed to meet the applicable requirements of this section. Each plan must be supported by appropriate engineering calculations. The owner or operator has completed the initial run-on and run-off control system plan when the plan has been placed in the facility's operating record as required by §257.105(g)(3).

This document and all attachments serve as the initial Run-on Run-off Control Plan and will be placed in the facility's operating record. Periodic Run-on and Run-off control plans will be prepared at 5-year increments or whenever determined necessary if there is a change in conditions that would affect the Plan.

<u>§257.81(c)(2)</u>: Amendment of the plan. The owner or operator may amend the written run-on and runoff control plan at any time provided the revised plan is placed in the facility's operating record as required by §257.105 (g) (3). The owner or operator must amend the written run-on and run-off control system plan whenever there is a change in conditions that would substantially affect the written plan in effect.

The Run-on and Run-off Control Plan will be amended if conditions change that substantially affect the written plan in effect. Any amendments to the Plan will include written certification from a qualified professional engineer that any amendments to the Plan meet the requirements of the CCR Rule.

A record of amendments to the Plan will be tracked below. The latest version of the Run-on and Run-off Control Plan will be noted on the first page of the Plan.

Version	Date	Description of Changes Made
1	16 October 2016	Initial Submittal

<u>§257.81(c)(3)</u>: Timeframes for preparing the initial plan

(i) Existing CCR landfills. The owner or operator of the CCR unit must prepare an initial run-on and run-off control system plan no later than October 17, 2016

The Run-on and Run-off Control Plan has been prepared within the specified time.



(ii) New CCR landfills and any lateral expansion of a CCR landfill. The owner or operator must prepare the initial run-on and run-off control system plan no later than the date of initial receipt of CCR in the CCR unit.

Not Applicable. This Plan will also be updated when existing phases of the landfill that are not actively receiving CCRs begin to receive CCRs.

<u>§257.81(c)(4)</u>: Frequency of revising the plan. The owner or operator of a CCR unit must prepare periodic run-on and run-off control system plans required by paragraph (c)(1) of this section every five years. The date of completing the initial plan is the basis for establishing the deadline to complete the first subsequent plan. The owner or operator may complete any required plan prior to the required deadline provided the owner or operator places the completed plan into the facility's operating record within a reasonable amount of time. In all cases, the deadline for completing a subsequent plan is based on the date of completing the previous plan. For purposes of this paragraph (c)(4), the owner or operator has completed a periodic run-on and run-off control system plan when the plan has been placed in the facility's operating record as required by §257.105(g)(3).

The Run-on and Run-off Control System Plan or any subsequent Plan will be assessed and amended whenever there is a change in operation of the CCR landfill that would substantially affect the Run-on and Run-off Control System Plan or when unanticipated events necessitate a revision of the Plan.

Professional Engineer Certification

<u>\$257.81(c)(5)</u>: The owner or operator must obtain a certification from a qualified professional engineer stating that the initial and periodic run-on and run-off control system plans meet the requirements of this section.

I certify that the above-referenced initial Run-on and Run-off Control System Plan for AECI's Utility Waste Landfill at the New Madrid Power Plant (NMPP) meets the USEPA's CCR Rule requirements of §257.81.

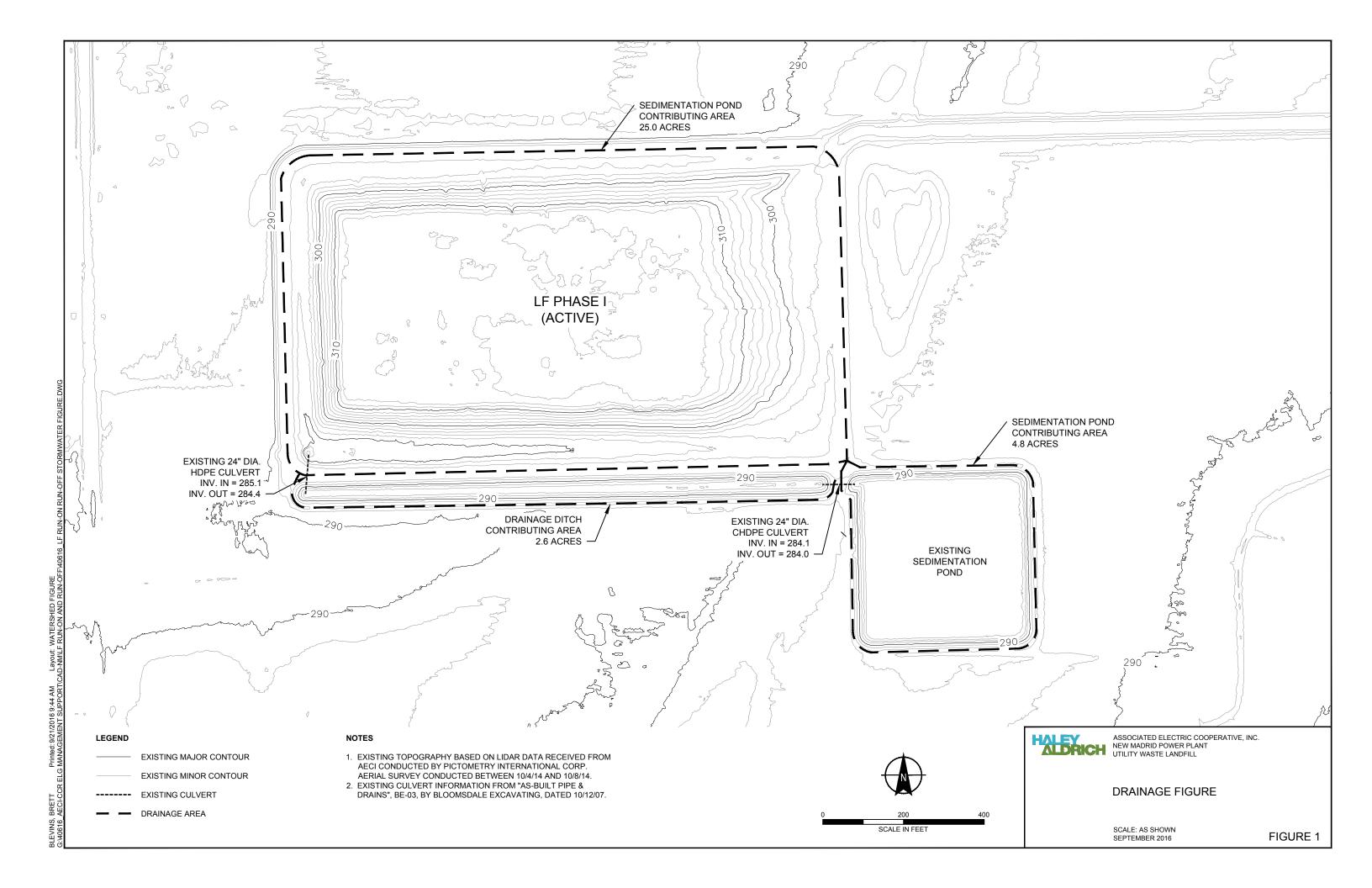
Certifying Engineer

Print Name: Missouri License No.: Title: Company: <u>Steven F. Putrich</u> 2014035813 <u>Project Principal</u> Haley & Aldrich, Inc.

Professional Engineer's Seal:

Signed:





> Appendix A NOAA Rainfall Data



Precipitation Frequency Data Server



NOAA Atlas 14, Volume 8, Version 2 Location name: Portageville, Missouri, US* Latitude: 36.4945°, Longitude: -89.5877° Elevation: 312 ft* * source: Google Maps



POINT PRECIPITATION FREQUENCY ESTIMATES

Sanja Perica, Deborah Martin, Sandra Pavlovic, Ishani Roy, Michael St. Laurent, Carl Trypaluk, Dale Unruh, Michael Yekta, Geoffery Bonnin

NOAA, National Weather Service, Silver Spring, Maryland

PF_tabular | PF_graphical | Maps_&_aerials

PF tabular

PDS-based point precipitation frequency estimates with 90% confidence intervals (in inches) ¹										
Duration	Average recurrence interval (years) 1 2 5 10 25 50 100 200 500 1000									
			-							
5-min	0.412 (0.329-0.515)	0.476 (0.379-0.596)	0.582 (0.462-0.729)	0.670 (0.530-0.842)	0.792 (0.609-1.02)	0.888 (0.668-1.15)	0.984 (0.719-1.29)	1.08 (0.762-1.45)	1.21 (0.825-1.66)	1.31 (0.873-1.81)
10-min	0.603 (0.481-0.754)	0.697 (0.556-0.872)	0.851 (0.677-1.07)	0.981 (0.776-1.23)	1.16 (0.891-1.49)	1.30 (0.978-1.68)	1.44 (1.05-1.90)	1.58 (1.12-2.12)	1.77 (1.21-2.42)	1.92 (1.28-2.65)
15-min	0.735 (0.587-0.920)	0.850 (0.678-1.06)	1.04 (0.826-1.30)	1.20 (0.946-1.50)	1.42 (1.09-1.82)	1.58 (1.19-2.05)	1.76 (1.28-2.31)	1.93 (1.36-2.59)	2.17 (1.47-2.96)	2.34 (1.56-3.23)
30-min	1.05 (0.840-1.32)	1.22 (0.974-1.53)	1.50 (1.19-1.88)	1.73 (1.37-2.17)	2.04 (1.57-2.62)	2.29 (1.72-2.97)	2.54 (1.85-3.34)	2.79 (1.96-3.74)	3.12 (2.13-4.26)	3.38 (2.25-4.66)
60-min	1.39 (1.11-1.74)	1.60 (1.28-2.00)	1.96 (1.56-2.46)	2.26 (1.79-2.84)	2.69 (2.07-3.46)	3.03 (2.28-3.93)	3.37 (2.47-4.45)	3.73 (2.63-5.01)	4.22 (2.88-5.77)	4.60 (3.06-6.35)
2-hr	1.73 (1.39-2.13)	1.98 (1.60-2.45)	2.42 (1.95-3.00)	2.79 (2.24-3.47)	3.33 (2.60-4.25)	3.76 (2.87-4.84)	4.21 (3.12-5.50)	4.68 (3.34-6.22)	5.32 (3.67-7.21)	5.82 (3.92-7.96)
3-hr	1.95 (1.59-2.39)	2.23 (1.81-2.74)	2.71 (2.20-3.34)	3.14 (2.53-3.87)	3.75 (2.95-4.76)	4.25 (3.27-5.44)	4.78 (3.57-6.21)	5.33 (3.84-7.07)	6.11 (4.24-8.24)	6.72 (4.55-9.13)
6-hr	2.38 (1.96-2.88)	2.71 (2.23-3.29)	3.29 (2.70-4.00)	3.81 (3.11-4.64)	4.56 (3.64-5.74)	5.19 (4.05-6.57)	5.85 (4.42-7.53)	6.55 (4.77-8.60)	7.54 (5.30-10.1)	8.32 (5.70-11.2)
12-hr	2.87 (2.39-3.43)	3.28 (2.73-3.93)	3.99 (3.31-4.78)	4.61 (3.81-5.55)	5.52 (4.46-6.85)	6.27 (4.95-7.84)	7.05 (5.39-8.97)	7.88 (5.81-10.2)	9.04 (6.43-12.0)	9.96 (6.90-13.3)
24-hr	3.40 (2.87-4.02)	3.92 (3.31-4.63)	4.79 (4.03-5.67)	5.54 (4.64-6.59)	6.62 (5.39-8.09)	7.48 (5.96-9.22)	8.37 (6.47-10.5)	9.30 (6.92-11.9)	10.6 (7.60-13.8)	11.6 (8.11-15.3)
2-day	3.98 (3.40-4.64)	4.61 (3.94-5.38)	5.67 (4.83-6.63)	6.56 (5.56-7.69)	7.80 (6.42-9.39)	8.78 (7.08-10.7)	9.78 (7.63-12.1)	10.8 (8.12-13.6)	12.2 (8.83-15.7)	13.2 (9.37-17.3)
3-day	4.37 (3.77-5.06)	5.06 (4.36-5.86)	6.20 (5.32-7.19)	7.16 (6.12-8.34)	8.51 (7.05-10.2)	9.56 (7.76-11.5)	10.6 (8.36-13.1)	11.7 (8.89-14.7)	13.2 (9.66-16.9)	14.4 (10.2-18.6)
4-day	4.68 (4.05-5.38)	5.40 (4.67-6.22)	6.60 (5.70-7.62)	7.62 (6.54-8.82)	9.04 (7.54-10.7)	10.2 (8.30-12.2)	11.3 (8.95-13.8)	12.5 (9.52-15.6)	14.1 (10.4-18.0)	15.3 (11.0-19.8)
7-day	5.40 (4.73-6.15)	6.19 (5.42-7.06)	7.53 (6.57-8.60)	8.68 (7.53-9.94)	10.3 (8.70-12.1)	11.6 (9.58-13.8)	12.9 (10.3-15.7)	14.3 (11.0-17.8)	16.2 (12.0-20.5)	17.7 (12.8-22.6)
10-day	6.07 (5.35-6.86)	6.92 (6.09-7.83)	8.35 (7.33-9.46)	9.57 (8.37-10.9)	11.3 (9.62-13.3)	12.7 (10.6-15.0)	14.2 (11.4-17.1)	15.7 (12.1-19.3)	17.7 (13.2-22.3)	19.3 (14.1-24.6)
20-day	8.17 (7.30-9.11)	9.15 (8.17-10.2)	10.8 (9.59-12.1)	12.1 (10.8-13.6)	14.1 (12.1-16.2)	15.6 (13.1-18.1)	17.1 (13.9-20.3)	18.6 (14.6-22.6)	20.7 (15.7-25.8)	22.4 (16.5-28.1)
30-day	9.98 (8.99-11.0)	11.1 (10.0-12.3)	12.9 (11.6-14.3)	14.4 (12.9-16.1)	16.5 (14.2-18.8)	18.0 (15.3-20.8)	19.6 (16.1-23.0)	21.1 (16.7-25.4)	23.2 (17.6-28.6)	24.7 (18.4-30.9)
45-day	12.3 (11.2-13.5)	13.6 (12.4-15.0)	15.8 (14.3-17.4)	17.5 (15.8-19.4)	19.8 (17.2-22.3)	21.5 (18.3-24.5)	23.1 (19.0-26.9)	24.7 (19.6-29.4)	26.6 (20.4-32.5)	28.1 (21.0-34.9)
60-day	14.2 (13.0-15.6)	15.8 (14.5-17.3)	18.3 (16.7-20.1)	20.3 (18.4-22.3)	22.8 (19.9-25.5)	24.6 (21.1-27.9)	26.3 (21.8-30.4)	28.0 (22.3-33.1)	29.9 (23.0-36.3)	31.3 (23.5-38.7)

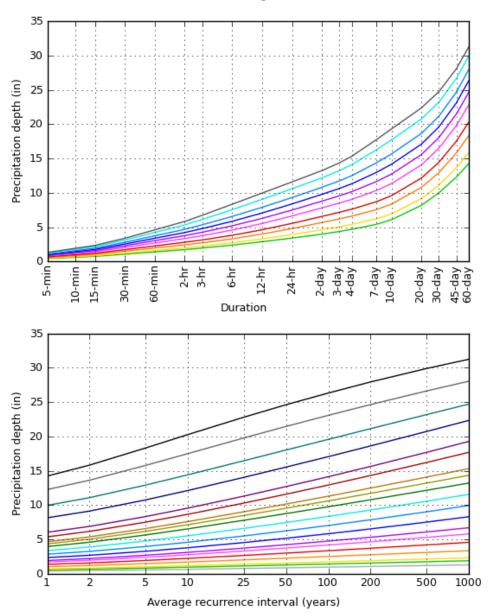
¹ Precipitation frequency (PF) estimates in this table are based on frequency analysis of partial duration series (PDS).

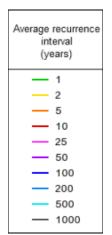
Numbers in parenthesis are PF estimates at lower and upper bounds of the 90% confidence interval. The probability that precipitation frequency estimates (for a given duration and average recurrence interval) will be greater than the upper bound (or less than the lower bound) is 5%. Estimates at upper bounds are not checked against probable maximum precipitation (PMP) estimates and may be higher than currently valid PMP values. Please refer to NOAA Atlas 14 document for more information.

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PF graphical

PDS-based depth-duration-frequency (DDF) curves Latitude: 36.4945°, Longitude: -89.5877°





NOAA Atlas 14, Volume 8, Version 2

Created (GMT): Mon Feb 23 19:19:49 2015

Duration							
— 5-min	2-day						
10-min	— 3-day						
15-min	- 4-day						
30-min	- 7-day						
- 60-min	— 10-day						
— 2-hr	- 20-day						
— 3-hr	— 30-day						
— 6-hr	— 45-day						
- 12-hr	- 60-day						
24-hr							

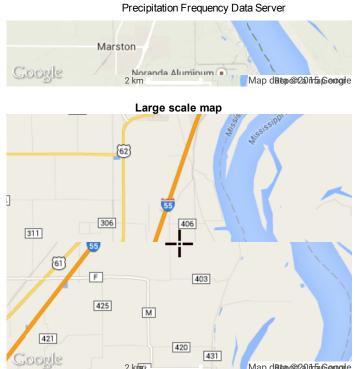
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Maps & aerials

Small scale terrain



Large scale terrain



Map date @ 220 it fa Georgie

Large scale aerial

2 km



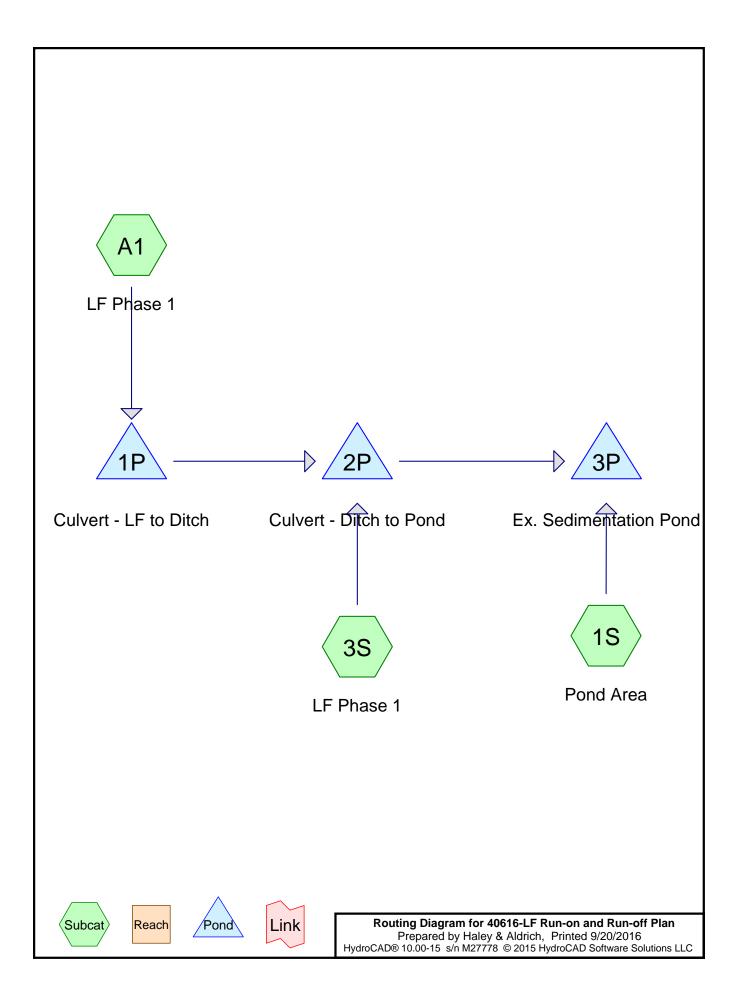
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US Department of Commerce National Oceanic and Atmospheric Administration National Weather Service Office of Hydrologic Development 1325 East West Highway Silver Spring, MD 20910 Questions?: <u>HDSC.Questions@noaa.gov</u>

Disclaimer

> Appendix B HydroCAD Results





Prepared by Haley & Aldrich HydroCAD® 10.00-15 s/n M27778 © 2015 HydroCAD Software Solutions LLC

Area Listing (all nodes)

Area	CN	Description
(acres)		(subcatchment-numbers)
2.618	98	(3S)
25.000	89	(A1)
4.766	98	Water Surface, HSG A (1S)
32.384	91	TOTAL AREA

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Soil Listing (all nodes)

Area	Soil	Subcatchment
(acres)	Group	Numbers
4.766	HSG A	1S
0.000	HSG B	
0.000	HSG C	
0.000	HSG D	
27.618	Other	3S, A1
32.384		TOTAL AREA

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Ground Covers (all nodes)

HSG-A	HSG-B	HSG-C	HSG-D	Other	Total	Ground	Subcatchment
 (acres)	(acres)	(acres)	(acres)	(acres)	(acres)	Cover	Numbers
 0.000	0.000	0.000	0.000	27.618	27.618		3S, A1
4.766	0.000	0.000	0.000	0.000	4.766	Water Surface	1S
4.766	0.000	0.000	0.000	27.618	32.384	TOTAL AREA	

Prepared by Haley & Aldrich

HydroCAD® 10.00-15 s/n M27778 © 2015 HydroCAD Software Solutions LLC

Line#	Node Number	In-Invert (feet)	Out-Invert (feet)	Length (feet)	Slope (ft/ft)	n	Diam/Width (inches)	Height (inches)	Inside-Fill (inches)
 1	1P	285.10	284.40	96.3	0.0073	0.013	24.0	0.0	0.0
2	2P	284.10	284.00	80.0	0.0013	0.013	24.0	0.0	0.0

Pipe Listing (all nodes)

Time span=0.00-36.00 hrs, dt=0.01 hrs, 3601 points Runoff by SCS TR-20 method, UH=SCS, Weighted-CN Reach routing by Dyn-Stor-Ind method - Pond routing by Dyn-Stor-Ind method

Subcatchment1S: Pond Area	Runoff Area=4.766 ac 100.00% Impervious Runoff Depth=6.38" Tc=0.0 min CN=98 Runoff=53.52 cfs 2.534 af
Subcatchment 3S: LF Phase 1	Runoff Area=2.618 ac 100.00% Impervious Runoff Depth=6.38" Tc=0.0 min CN=98 Runoff=29.40 cfs 1.392 af
Subcatchment A1: LF Phase 1 Flow	Runoff Area=25.000 ac 0.00% Impervious Runoff Depth=5.34" Length=1,954' Tc=26.7 min CN=89 Runoff=120.93 cfs 11.120 af
	eak Elev=292.62' Storage=154,800 cf Inflow=120.93 cfs 11.120 af Culvert n=0.013 L=96.3' S=0.0073 '/' Outflow=26.41 cfs 11.120 af
Pond 2P: Culvert - Ditch to Pond 24.0" Round (Peak Elev=288.38' Storage=95,302 cf Inflow=47.38 cfs 12.512 af Culvert n=0.013 L=80.0' S=0.0013 '/' Outflow=21.64 cfs 12.432 af
Pond 3P: Ex. Sedimentation Pond	Peak Elev=285.05' Storage=781,897 cf Inflow=66.99 cfs 14.966 af Outflow=0.98 cfs 2.369 af
Total Runoff Area = 32.384 a	c Runoff Volume = 15.047 af Average Runoff Depth = 5.58"

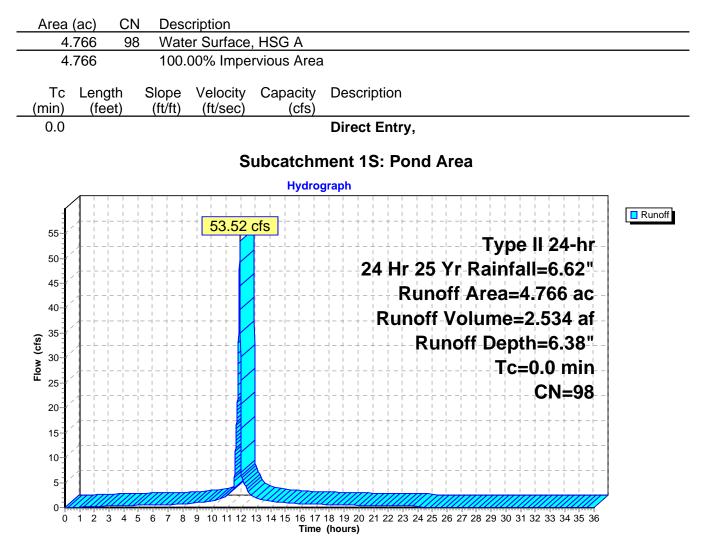
77.20% Pervious = 25.000 ac 22.80% Impervious = 7.384 ac

Summary for Subcatchment 1S: Pond Area

[46] Hint: Tc=0 (Instant runoff peak depends on dt)

Runoff = 53.52 cfs @ 11.90 hrs, Volume= 2.534 af, Depth= 6.38"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-36.00 hrs, dt= 0.01 hrs Type II 24-hr 24 Hr 25 Yr Rainfall=6.62"

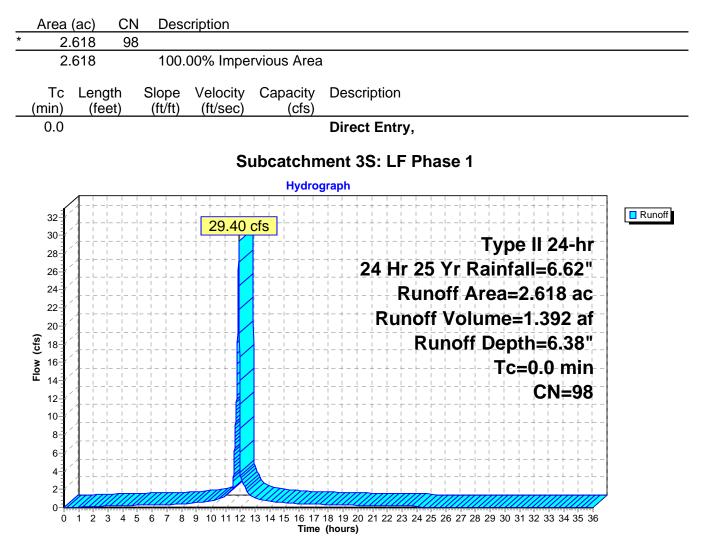


Summary for Subcatchment 3S: LF Phase 1

[46] Hint: Tc=0 (Instant runoff peak depends on dt)

Runoff = 29.40 cfs @ 11.90 hrs, Volume= 1.392 af, Depth= 6.38"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-36.00 hrs, dt= 0.01 hrs Type II 24-hr 24 Hr 25 Yr Rainfall=6.62"



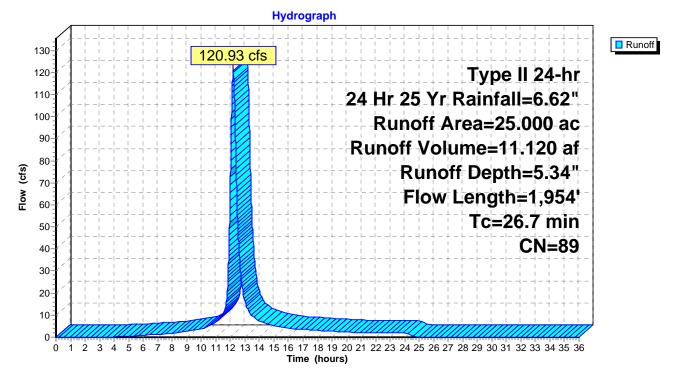
Summary for Subcatchment A1: LF Phase 1

120.93 cfs @ 12.19 hrs, Volume= 11.120 af, Depth= 5.34" Runoff =

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-36.00 hrs, dt= 0.01 hrs Type II 24-hr 24 Hr 25 Yr Rainfall=6.62"

_	Area	(ac) C	N Desc	cription		
*	25.	3 000	39			
	25.000		100.00% Pervious Area		ous Area	
	Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
	2.4	214	0.0133	1.51		Sheet Flow,
	0.5	447	0 4700	0.70		Smooth surfaces n= 0.011 P2= 3.92"
	0.5	117	0.1700	3.70		Sheet Flow, Smooth surfaces n= 0.011 P2= 3.92"
	23.8	1,623	0.0050	1.14		Shallow Concentrated Flow, Unpaved Kv= 16.1 fps
	26.7	1,954	Total			

Subcatchment A1: LF Phase 1



Summary for Pond 1P: Culvert - LF to Ditch

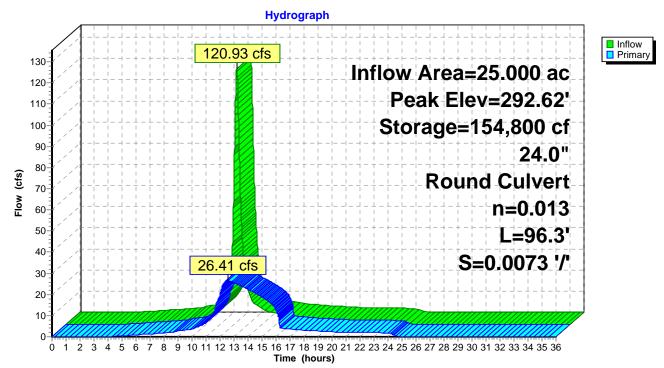
Inflow Area	a =	25.000 ac,	0.00% Impervious, Inflow	Depth = 5.34" for 24 Hr 25 Yr event	
Inflow	=	120.93 cfs @	12.19 hrs, Volume=	11.120 af	
Outflow	=	26.41 cfs @	12.54 hrs, Volume=	11.120 af, Atten= 78%, Lag= 20.7 m	in
Primary	=	26.41 cfs @	12.54 hrs, Volume=	11.120 af	

Routing by Dyn-Stor-Ind method, Time Span= 0.00-36.00 hrs, dt= 0.01 hrs Peak Elev= 292.62' @ 12.75 hrs Surf.Area= 86,465 sf Storage= 154,800 cf

Plug-Flow detention time= 43.3 min calculated for 11.120 af (100% of inflow) Center-of-Mass det. time= 43.2 min (844.1 - 800.9)

Volume	Inve	ert Avail.Sto	orage	Storage	Description	
#1	285.0	00' 320,4	63 cf	Custom	Stage Data (Pi	rismatic)Listed below (Recalc)
Flovetia			امد	Chara	Curra Chara	
Elevatio		Surf.Area		Store	Cum.Store	
(fee	et)	(sq-ft)	(cubic	:-teet)	(cubic-feet)	
285.0	00	0		0	0	
286.0	00	63		32	32	
287.0	00	234		149	180	
288.0	00	441		338	518	
289.0	00	8,791		4,616	5,134	
290.0	00	25,092	10	6,942	22,075	
291.0	00	42,540	3	3,816	55,891	
292.0	00	62,635	52	2,588	108,479	
293.0	00	100,988	8	1,812	190,290	
294.0	00	159,357	13	0,173	320,463	
Device	Routing	Invert	Outle	et Device	S	
#1	Primary	285.10'	24.0"	' Round	Culvert	
			L= 96	5.3' CPF	P, projecting, no	headwall, Ke= 0.900
						284.40' S= 0.0073 '/' Cc= 0.900
						ooth interior, Flow Area= 3.14 sf
					J	,

Primary OutFlow Max=26.38 cfs @ 12.54 hrs HW=292.54' TW=287.66' (Dynamic Tailwater) ☐ 1=Culvert (Inlet Controls 26.38 cfs @ 8.40 fps)



Pond 1P: Culvert - LF to Ditch

Summary for Pond 2P: Culvert - Ditch to Pond

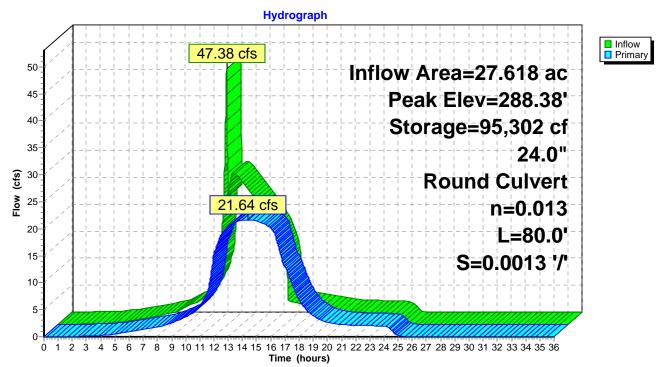
Inflow Area =	=	27.618 ac,	9.48% Impervious, Inflow	Depth = 5.44" for 24 Hr 25 Yr event
Inflow =	=	47.38 cfs @	11.90 hrs, Volume=	12.512 af
Outflow =	=	21.64 cfs @	14.40 hrs, Volume=	12.432 af, Atten= 54%, Lag= 149.9 min
Primary =	=	21.64 cfs @	14.40 hrs, Volume=	12.432 af

Routing by Dyn-Stor-Ind method, Time Span= 0.00-36.00 hrs, dt= 0.01 hrs Peak Elev= 288.38' @ 14.40 hrs Surf.Area= 39,851 sf Storage= 95,302 cf

Plug-Flow detention time= 59.7 min calculated for 12.432 af (99% of inflow) Center-of-Mass det. time= 55.7 min (887.6 - 831.8)

Volume	Inve	ert Avail.Sto	brage Storage Description				
#1	284.0	00' 360,9	59 cf Custo	m Stage Data (Prism	atic)Listed below (Recalc)		
Flovetia	~	Surf Area	Inc Store	Cum Store			
Elevatio		Surf.Area	Inc.Store	Cum.Store			
(fee	t)	(sq-ft)	(cubic-feet)	(cubic-feet)			
284.0	0	0	0	0			
285.0	0	10,595	5,298	5,298			
286.00		21,636	16,116	21,413			
287.00		29,788	25,712	47,125			
288.00		37,073	33,431	80,556			
289.00		44,319	40,696	121,252			
290.00		51,733	48,026	169,278			
291.00		59,757	55,745	225,023			
292.00		67,956	63,857	288,879			
293.00		76,204	72,080	360,959			
Device	Routing	Invert	Outlet Devi	ces			
#1	Primary	284.10'	24.0" Round Culvert				
			L= 80.0' CPP, projecting, no headwall, Ke= 0.900				
Inlet / Outlet Invert= 284.10' / 284.00' S= 0.0013 '/' Cc= (
n= 0.013 Corrugated PE, smooth interior, Flow							
				onagatoa r E, onooth			

Primary OutFlow Max=21.64 cfs @ 14.40 hrs HW=288.38' TW=283.29' (Dynamic Tailwater) ☐ 1=Culvert (Inlet Controls 21.64 cfs @ 6.89 fps)



Pond 2P: Culvert - Ditch to Pond

Summary for Pond 3P: Ex. Sedimentation Pond

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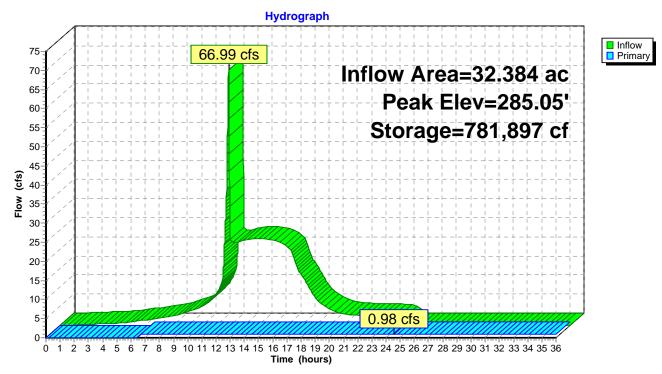
Inflow Area =	32.384 ac, 22.80% Impervious, Inflow Depth > 5.55" for 24 Hr 25 Yr event
Inflow =	66.99 cfs @ 11.90 hrs, Volume= 14.966 af
Outflow =	0.98 cfs @ 24.60 hrs, Volume= 2.369 af, Atten= 99%, Lag= 762.1 min
Primary =	0.98 cfs @ 24.60 hrs, Volume= 2.369 af

Routing by Dyn-Stor-Ind method, Time Span= 0.00-36.00 hrs, dt= 0.01 hrs Starting Elev= 281.00' Surf.Area= 133,951 sf Storage= 196,036 cf Peak Elev= 285.05' @ 24.60 hrs Surf.Area= 157,710 sf Storage= 781,897 cf (585,862 cf above start)

Plug-Flow detention time= (not calculated: initial storage exceeds outflow) Center-of-Mass det. time= 417.4 min (1,278.9 - 861.5)

Volume	Inv	ert Avail.Sto	rage Storage	e Description			
#1	279.5	50' 1,263,3	71 cf Custor	n Stage Data (Pi	rismatic)Listed below (Recalc)		
Elevatio		Surf.Area	Inc.Store	Cum.Store			
(fee	t)	(sq-ft)	(cubic-feet)	(cubic-feet)			
279.5	0	127,449	0	0			
280.0	0	129,597	64,262	64,262			
281.0	0	133,951	131,774	196,036			
282.0	0	138,367	136,159	332,195			
283.0	0	142,847	140,607	472,802			
284.0	0	151,086	146,967	619,768			
285.0	0	157,516	154,301	774,069			
286.0	0	161,415	159,466	933,535			
287.0	0	164,847	163,131	1,096,666			
288.0	0	168,564	166,706	1,263,371			
Device	Routing	Invert	Outlet Device	26			
-							
#1	Primary	281.10'	Pump	207 00' Turna (284 00		
Discharges@307.00' Turns Off@281.00'							
6.0" Diam. x 8,413.0' Long Discharge, Hazen-							
			Flow (gpm)=	= 100.0 200.0 3	00.0 400.0 500.0 600.0 700.0 800.0		
Head (feet)= 156.00 154.00 150.00 144.00 137.00 122.00 105.00 72.00							
			-Loss (feet)= 7.65 27.62 58.52 99.70 150.72 211.25 281.04 359.88				
			=Lift (feet)= -287.88	148.35 126.38	3 91.48 44.30 -13.72 -89.25 -176.04		
Driver Out Flow Mars 0.00 of @ 04.00 hrs. LIVA 005.051 (Free Discharge)							

Primary OutFlow Max=0.98 cfs @ 24.60 hrs HW=285.05' (Free Discharge)



Pond 3P: Ex. Sedimentation Pond